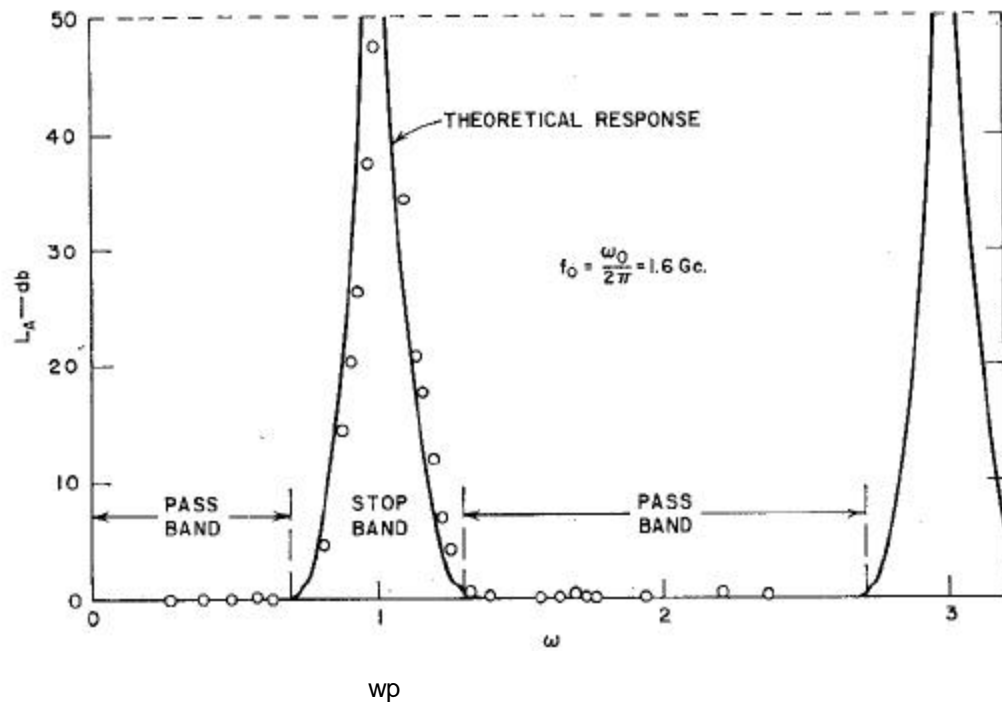
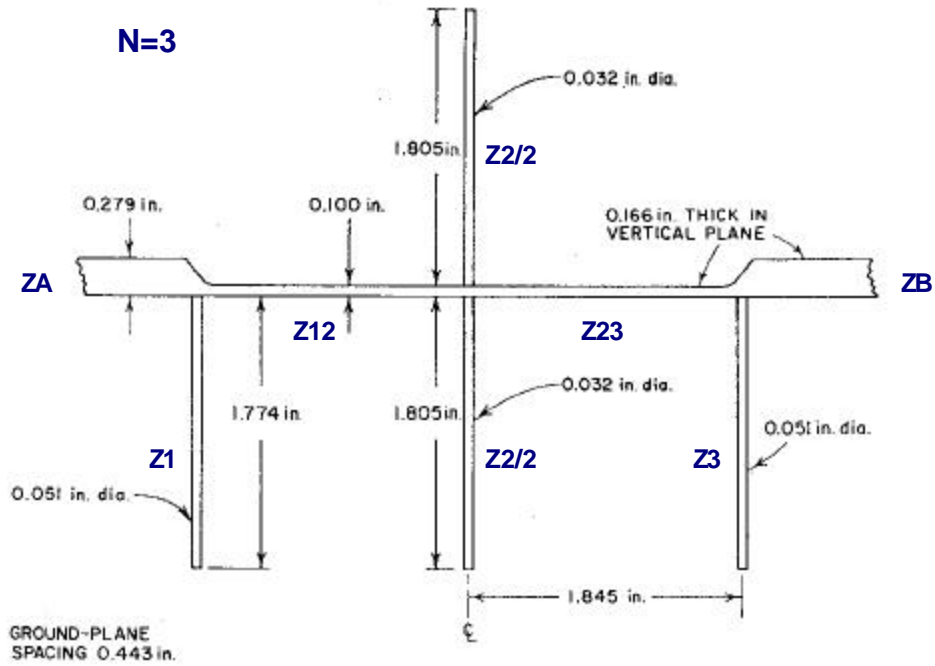


Microwave Notch Filter Design Sheet

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This sheet calculates a stop-band filter according to Schiffman and Matthaei, IEEE trans MTT, January 1962. page 6.



There are three steps to this notch filter:

Step 1, Get the filter g-values, this sheet calculated the g values according to the Chebychev polynomial for a given N, but these can be obtained in a variety of ways from books or from a program freely available from this web page.

Step 2, Calculate Zo for the filter (this sheet stops there). All section are lambda/4

Step 3, Calculate length and width. One method is to use Linecalc which is part of ADS. For microstrip designs I have written a MathCAD sheet which is available from my wepage that works well for thin tracks, less well for thicker tracks. Also you can try transcalc.sourceforge.net for a Linecalc equivalent.

Yellow is user input, Green is output

$$\mu\text{m} := 10^{-6} \cdot \text{m} \quad \text{nH} := 10^{-9} \cdot \text{henry}$$

Main user input area:

$L_{\text{ar_db}} := 0.1$ Passband ripple in dB for the chebchev calculations

$N := 5$ Order of the filter 1 to 5, please choose correct section below for the results

$f_0 := 1.6 \cdot \text{GHz}$ $f_{\text{bw}} := f_0 \cdot 0.6$ $Z_A := 50 \cdot \Omega$ $\omega_p := 1.0$

refer to frequency repetition above. If you need to attenuate signal and all harmonics set to 1.5

Calculate Chebychev (g) Polynomials

$$k := 1..N \quad \beta := \ln\left(\coth\left(\frac{L_{\text{ar_db}}}{17.37}\right)\right) \quad \gamma := \sinh\left(\frac{\beta}{2 \cdot N}\right) \quad a_k := \sin\left[\frac{(2 \cdot k - 1) \cdot \pi}{2 \cdot N}\right]$$

$$b_k := \gamma^2 + \left(\sin\left(\frac{k \cdot \pi}{N}\right)\right)^2 \quad g_k := 0$$

$$g_0 := 1$$

$$g_{N+1} := 1$$

$g(0)$ and $g(N+1)$ represent the input/output coupling for odd order filters, these are 1 representing the generator (and equal) load resistance

$$g_k := \begin{cases} \frac{2 \cdot a_1}{\gamma} & \text{if } k = 1 \\ \frac{4 \cdot a_{k-1} \cdot a_k}{b_{k-1} \cdot g_{k-1}} & \text{otherwise} \end{cases}$$

$$g = \begin{pmatrix} 1 \\ 1.147 \\ 1.371 \\ 1.975 \\ 1.371 \\ 1.147 \\ 1 \end{pmatrix}$$

Calculate basic factors

$$f_1 := f_0 - \frac{f_{\text{bw}}}{2} \quad a := \cot\left(\frac{\pi \cdot f_1}{2 \cdot f_0}\right) \quad \Lambda := \omega_p \cdot a$$

$$f_1 = 1.12 \text{ GHz}$$

$$a = 0.509525$$

$$\Lambda = 0.509525$$

For N=1. Note the input and output impedances are different

$$N1_Z1 := \frac{Z_A}{\Lambda \cdot g_0 \cdot g_1} \quad N1_ZB := \frac{Z_A \cdot g_2}{g_0}$$

$$N1_Z1 = 85.566 \text{ ohm}$$

$$N1_ZB = 68.56 \text{ ohm}$$

For N=2

$$N2_Z1 := Z_A \cdot \left(1 + \frac{1}{\Lambda \cdot g_0 \cdot g_1} \right) \quad N2_Z12 := Z_A \cdot (1 + \Lambda \cdot g_0 \cdot g_1)$$

$$N2_Z1 = 135.566 \text{ ohm}$$

$$N2_Z12 = 79.217 \text{ ohm}$$

$$N2_Z2 := \frac{Z_A \cdot g_0}{\Lambda \cdot g_2} \quad N2_ZB := Z_A \cdot g_0 \cdot g_3$$

$$N2_Z2 = 71.565 \text{ ohm}$$

$$N2_ZB = 98.751 \text{ ohm}$$

For N=3

$$N3_Z1 := Z_A \cdot \left(1 + \frac{1}{\Lambda \cdot g_0 \cdot g_1} \right) \quad N3_Z12 := Z_A \cdot (1 + \Lambda \cdot g_0 \cdot g_1)$$

$$N3_Z1 = 135.566 \text{ ohm}$$

$$N3_Z12 = 79.217 \text{ ohm}$$

$$N3_Z2 := \frac{Z_A \cdot g_0}{\Lambda \cdot g_2} \quad N3_Z3 := \frac{Z_A \cdot g_0}{g_4} \cdot \left(1 + \frac{1}{\Lambda \cdot g_0 \cdot g_4} \right)$$

$$N3_Z2 = 71.565 \text{ ohm}$$

$$N3_Z23 := \frac{Z_A \cdot g_0}{g_4} \cdot (1 + \Lambda \cdot g_0 \cdot g_1) \quad N3_ZB := \frac{Z_A \cdot g_0}{g_4}$$

$$N3_Z23 = 57.772 \text{ ohm}$$

$$N3_Z3 = 88.655 \text{ ohm}$$

$$N3_ZB = 36.464 \text{ ohm}$$

For N=4

$$N4_Z1 := Z_A \cdot \left(2 + \frac{1}{\Lambda \cdot g_0 \cdot g_1} \right) \quad N4_Z12 := Z_A \cdot \left(\frac{1 + 2 \cdot \Lambda \cdot g_0 \cdot g_1}{1 + \Lambda \cdot g_0 \cdot g_1} \right)$$

$$N4_Z2 := Z_A \cdot \left[\frac{1}{1 + \Lambda \cdot g_0 \cdot g_1} + \frac{g_0}{\Lambda \cdot g_2 (1 + \Lambda \cdot g_0 \cdot g_1)^2} \right] \quad N4_Z23 := \frac{Z_A}{g_0} \cdot \left(\Lambda \cdot g_2 + \frac{g_0}{1 + \Lambda \cdot g_0 \cdot g_1} \right)$$

$$N4_Z3 := \frac{Z_A}{\Lambda \cdot g_0 \cdot g_3} \quad N4_Z34 := \frac{Z_A}{g_0 \cdot g_5} \cdot (1 + \Lambda \cdot g_4 \cdot g_5)$$

$$N4_Z1 = 185.566 \text{ ohm}$$

$$N4_Z4 := \frac{Z_A}{g_0 g_5} \cdot \left(1 + \frac{1}{\Lambda \cdot g_4 \cdot g_5} \right)$$

$$N4_ZB := \frac{Z_A}{g_0 g_5}$$

$$N4_Z12 = 68.441 \text{ ohm}$$

$$N4_Z2 = 60.069 \text{ ohm}$$

$$N4_Z23 = 66.492 \text{ ohm}$$

$$N4_Z4 = 98.01 \text{ ohm}$$

$$N4_Z3 = 49.686 \text{ ohm}$$

$$N4_ZB = 43.598 \text{ ohm}$$

$$N4_Z34 = 78.531 \text{ ohm}$$

For N=5

$$N5_Z1 := N4_Z1$$

$$N5_Z12 := N4_Z12$$

$$N5_Z2 := N4_Z2$$

$$N5_Z23 := N4_Z23$$

$$N5_Z3 := N4_Z3$$

$$N5_Z4 := \frac{Z_A}{g_0} \cdot \left[\frac{1}{1 + \Lambda \cdot g_5 \cdot g_6} + \frac{g_6}{\Lambda \cdot g_4 (1 + \Lambda \cdot g_4 \cdot g_5)^2} \right]$$

$$N5_Z34 := \frac{Z_A}{g_0} \cdot \left(\Lambda \cdot g_4 + \frac{g_6}{1 + \Lambda \cdot g_5 \cdot g_6} \right)$$

$$N5_Z5 := \frac{Z_A \cdot g_6}{g_0} \cdot \left(2 + \frac{1}{\Lambda \cdot g_5 \cdot g_6} \right)$$

$$N5_Z45 := \frac{Z_A \cdot g_6}{g_0} \cdot \left(\frac{1 + 2 \cdot \Lambda \cdot g_5 \cdot g_6}{1 + \Lambda \cdot g_5 \cdot g_6} \right)$$

$$N5_Z1 = 185.566 \text{ ohm}$$

$$N5_Z12 = 68.441 \text{ ohm}$$

$$N5_ZB := \frac{Z_A \cdot g_6}{g_0}$$

$$N5_Z4 = 53.616 \text{ ohm}$$

$$N5_Z2 = 60.069 \text{ ohm}$$

$$N5_Z45 = 68.441 \text{ ohm}$$

$$N5_Z23 = 66.492 \text{ ohm}$$

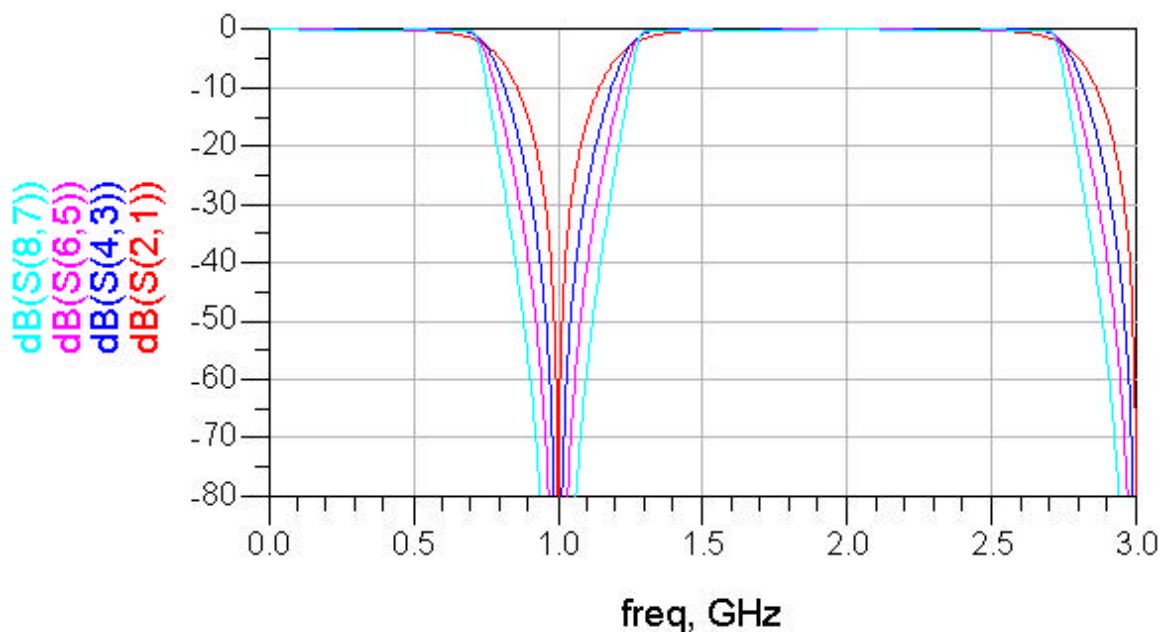
$$N5_Z5 = 185.566 \text{ ohm}$$

$$N5_Z3 = 49.686 \text{ ohm}$$

$$N5_ZB = 50 \text{ ohm}$$

$$N5_Z34 = 66.492 \text{ ohm}$$

Does it work?



The plots above are for four different notch filters from $n=2$ to $n=5$, simulated with ideal transmission lines shown below. Each line is 90 degrees at the wanted frequency, and the results are excellent

